

# CO<sub>2</sub> gas-activated sintering of carbonated hydroxyapatites

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## Abstract

Sintering compacts of carbonated hydroxyapatite (CHA) nanoparticles (3.4 wt% CO<sub>3</sub><sup>2-</sup>) in a CO<sub>2</sub> flow (4 mL/min) proceeded at a temperature which was more than 200 °C lower than that for hydroxyapatite in air (1150 °C). During heating from RT to 1200 °C (5 K/min) the rate of shrinkage of the CHA compacts showed a maximum thrice as high as that in air at about 929 °C. The shrinkage correlates with a mass loss caused by the release of CO<sub>2</sub> due to the thermal decomposition of CO<sub>3</sub><sup>2-</sup> ions that substitute PO<sub>4</sub><sup>3-</sup> ions in the CHA lattice. Firing the compacts in the CO<sub>2</sub> flow at 800 and 900 °C for 2 h resulted in an additional carbonation on the B-sites and a further decrease in the sintering temperature to 890 °C. The compacts fired in the 900–1000 °C range became almost complete ceramics with high densities and mechanical properties close to those of medical implants. Firing at temperatures above 1000 °C resulted in an additional carbonation on the A-sites. However, this led to a material with low densities and poor mechanical properties. A supposition has been proposed that the effect of CO<sub>2</sub> gas-activated sintering is a result of the intensification of the diffusion in the nanoparticles caused by CO<sub>2</sub> molecules entering the bulk from the CO<sub>2</sub> atmosphere and (or) releasing from the bulk due to the decomposition of carbonates on the B-sites in the lattice.

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## 1. Introduction

The carbonate ion, CO<sub>3</sub><sup>2-</sup>, is an important substitution in hydroxyapatite (HA), Ca<sub>10</sub>(PO<sub>4</sub>)<sub>6</sub>(OH)<sub>2</sub>, of biological origin and it is processed by wet precipitation. CO<sub>3</sub><sup>2-</sup> can substitute for OH<sup>-</sup>, PO<sub>4</sub><sup>3-</sup> or both resulting in A-type, AB-type or B-type carbonated hydroxyapatite (CHA), respectively.<sup>1,2</sup>

CHA ceramics have been studied comprehensively as prospective materials for orthopaedic, fluorescence and sensor applications.<sup>3–5</sup> However, some problems arose in processing CHA ceramics with the desired degree and mode (A-, AB- or B-types) of carbonation. The CO<sub>3</sub><sup>2-</sup> content in a ceramic was found to depend strongly on processing variables, mainly, on the CO<sub>3</sub><sup>2-</sup> content and structural state of the initial powder used for compacting, but also on temperature, heating rate, duration and atmosphere of sintering, and the mode of substitution changes unpredictably during the heat-treatment.<sup>6–15</sup> In general it can

be said that, the higher the CO<sub>3</sub><sup>2-</sup> content in an initial powder is, the lower is its crystallinity and sintering temperature and, as a result, the higher is the carbonation in the processed ceramics.<sup>9,10,12,13</sup> The use of CO<sub>2</sub> atmospheres (wet or dry) led to alterations in shrinkage rate and sintering temperature of the compacts and to changes in chemical and phase compositions and structural characteristics, like the type of carbonation, of CHA ceramics.<sup>3–5,8,11</sup>

The overall situation gets even more complicated if the initial powder includes other impurities besides CO<sub>3</sub><sup>2-</sup>. These stem usually from parent reagents, the synthesis reaction or powder-processing (like ions, intermediate phases or by-products, respectively). The impurities decompose and/or react in the lattice during heat-treating compacts of the powder.<sup>16</sup> These solid-state reactions highly affect the densification.<sup>17</sup>

After all, the sintering process of a CHA ceramic under the conditions described above has not yet been elucidated sufficiently. The aim of this study was to clarify the principal factors for lowering the sintering temperature and to reveal the role of CO<sub>2</sub> atmospheres for processing CHA ceramics with desired characteristics.

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## 2. Materials and methods

In order to exclude the effect of other ions except  $\text{CO}_3^{2-}$  on sintering CHA's, the following procedure was used.<sup>18</sup> Precipitates were produced by a wet method employing the reaction of calcium carbonate and orthophosphoric acid.<sup>19</sup> Because of the negligible solubility of  $\text{CaCO}_3$  in water,<sup>20</sup> the reaction was promoted by using a fine-grained  $\text{CaCO}_3$  powder and the synthesis was carried out at 45 °C, which is an elevated temperature for a wet method. After grinding, a specific amount of  $\text{CaCO}_3$  powder (Merck, Darmstadt, Germany, analytical grade) was dispersed in distilled water. A solution of  $\text{H}_3\text{PO}_4$  (Merck) was rapidly poured into the  $\text{CaCO}_3$  suspension under continuous mixing of the reaction medium.

The formed precipitate was centrifugalized, dried in an oven at 90 °C, ground in an agate mortar and sieved through a 100  $\mu\text{m}$  sieve resulting in the initial powder. Compacts were made as pellets of 3 mm height and 10 mm diameter by pressing portions of the powder in a steel die under 120 MPa. The average porosity of the compacts was  $51 \pm 0.5\%$ . The compacts were fired in a dry  $\text{CO}_2$  flow (4 mL/min) in the range of 800–1200 °C with a 100 °C step and 2 h dwell-time at each temperature. Five batches of fired compacts were prepared with 10 samples each.

Structural analysis was performed using a Philips APDW 40C diffractometer and a copper  $K_\alpha$  radiation ( $\lambda = 0.154 \text{ nm}$ ) with a nickel filter through 20–70° diffraction angles ( $2\theta$ ). IR spectra were recorded employing a BIO-RAD FFS 175 spectrometer (Germany) at a  $2 \text{ cm}^{-1}$  resolution and the KBr technique, operating in the transmittance mode between wave numbers of 400–4000  $\text{cm}^{-1}$ . The morphology and microstructure of the samples were studied using an ESEM Quanta 400 scanning electron microscope (Germany).

Calcium amounts in the samples were determined by atomic absorption spectroscopy (Thermo Electron Corporation, M-series AA spectrometer). Corresponding amounts of orthophosphate were found by colorimetry using the molybdenum blue method (Varian Cary Win UV spectrophotometer,  $\lambda = 725 \text{ nm}$ ).

A thermogravimetric (TG) study of the samples was conducted up to 1200 °C in a  $\text{N}_2$  flow of 50 mL/min (NETZSCH STA 409 PC/PG, Germany), air or a dry  $\text{CO}_2$  flow of about 4 mL/min (MVT Instrument, Ukraine) at a heating rate of 5 K/min with the absolute error of the measurement being 2%. The dynamic shrinkage in the compacts was measured by dilatometry (MVT Instrument, Ukraine) using the same heating rate and atmospheric conditions as in the thermogravimetric study.

The density of the samples was measured by the Archimedes' principle using distilled water and average values for 10 samples in each batch. The relative density and the apparent porosity were calculated using  $3.156 \text{ g/cm}^3$  as the theoretical density of stoichiometric HA. The error of the determination was less than 1%. The Vickers hardness of the fired compacts was determined using a PMT-3 microhardness tester (USSR) by applying an ultimate load of 2 N for 10 s. The compressive strength was measured employing an Instron-type testing machine.

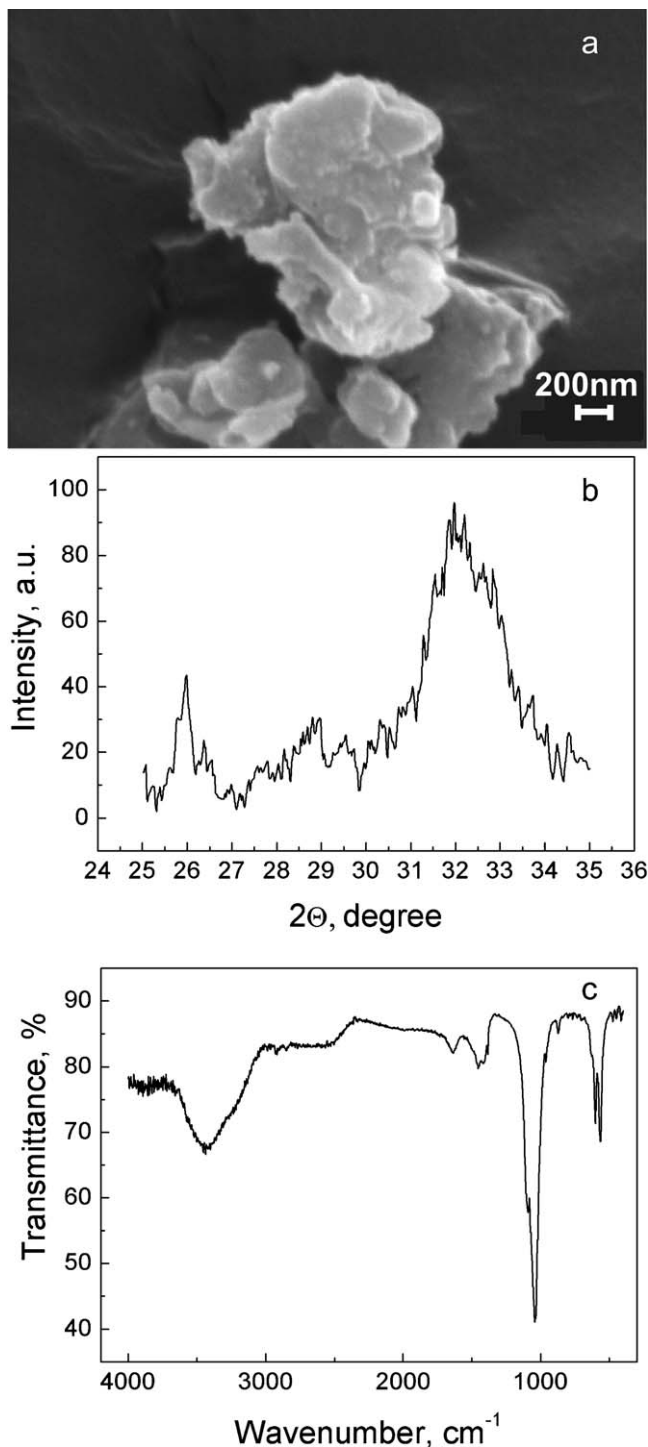


Fig. 1. Typical a – SEM micrograph, b – XRD pattern, and c – IR spectrum of the initial powder.

## 3. Results

### 3.1. Characterization of the initial powder

According to SEM pictures, the initial powder consists of particles with sizes in the wide range of 0.1–100  $\mu\text{m}$ . However, each particle is consisted from tiny platelets of around  $10^2 \text{ nm}$  (Fig. 1a). XRD patterns of the powder manifest

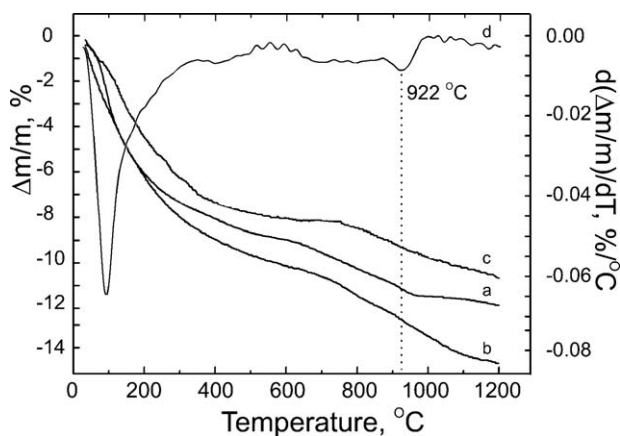


Fig. 2. TG curves of the initial powder in a – N<sub>2</sub> flow, b – air, and c – CO<sub>2</sub> flow; d – the DTG curve for the powder in the N<sub>2</sub> flow.

considerably broadened diffraction maxima positioned at diffraction angles  $2\theta$  as those of a nanocrystalline HA (Fig. 1b). IR spectra (Fig. 1c) show the absorption of PO<sub>4</sub><sup>3-</sup> ions at 566, 602, 962, 1042, 1090 cm<sup>-1</sup> and of lattice and adsorbed water at 1636 and 3440 cm<sup>-1</sup>, respectively. Very weak shoulders at 3570 and 630 cm<sup>-1</sup> indicate little amounts of OH<sup>-</sup> groups in the lattice, additionally absorptions at 1416 and 1452 cm<sup>-1</sup> of  $\nu_3$  CO<sub>3</sub><sup>2-</sup> groups and 875 cm<sup>-1</sup> of  $\nu_2$  CO<sub>3</sub><sup>2-</sup> are present. Traces of CO<sub>3</sub><sup>2-</sup> groups can be expected in a HA powder prepared by wet synthesis if no precaution for their elimination is taken.<sup>6,17</sup> Moreover, it is plausible to expect the presence of CO<sub>3</sub><sup>2-</sup> ions in the HA as residual precipitates stemming from the applied reaction since the ions are a constituent of the CaCO<sub>3</sub> reagent. A sharp but weak band at 1385 cm<sup>-1</sup> is associated with the NO<sub>3</sub><sup>-</sup> impurities of the KBr used for sample preparation in the IR study.

A TG curve in case of heating the powder in a N<sub>2</sub> flow has two plateau-like sections. The temperature ranges of the sections are determined from the corresponding DTG curve at about 520–600 °C and 980–1060 °C (Fig. 2a and d). Therefore, the TG curve is divided into three parts of room temperature (RT) to 600 °C, 600–1000 °C, and 1000–1200 °C. Considering the nature of the gases released from a powder processed by the “nitrous” method during heating<sup>21</sup> and the fact that only H<sub>2</sub>O and CO<sub>3</sub><sup>2-</sup> might have been the impurities in the powder prepared in this study, it can be concluded that adsorbed and lattice water liberated in the RT to 600 °C range, CO<sub>2</sub> in the 600–1000 °C range, and water due to the dehydroxylation in the N<sub>2</sub> flow at temperatures above 1000 °C. As a result, mass losses of 8.8 wt% for H<sub>2</sub>O (to 600 °C), 2.5 wt% for CO<sub>2</sub> (from 600 to 1000 °C), and 0.4 wt% for H<sub>2</sub>O (above 1000 °C) are calculated from the curve, giving a total mass loss of 11.7 wt%. The CO<sub>2</sub> mass loss of 2.5 wt% is caused by the thermal decomposition of 3.4 wt% CO<sub>3</sub><sup>2-</sup> in the lattice. This result is in acceptable agreement with an IR evaluation. Applying a calibration curve for a B-type CHA (CO<sub>3</sub><sup>2-</sup> content vs  $R_B = A_{1420}/A_{603}$ , where  $A_{1420}$  and  $A_{603}$  were  $\nu_3$  CO<sub>3</sub><sup>2-</sup> and  $\nu_4$  PO<sub>4</sub><sup>3-</sup> absorbencies, respectively),<sup>22</sup> a value of 3.2 wt% for CO<sub>3</sub><sup>2-</sup> in B position is found (for  $R_B = 0.47$  from the IR spectrum of the initial powder, Fig. 1c). In accordance

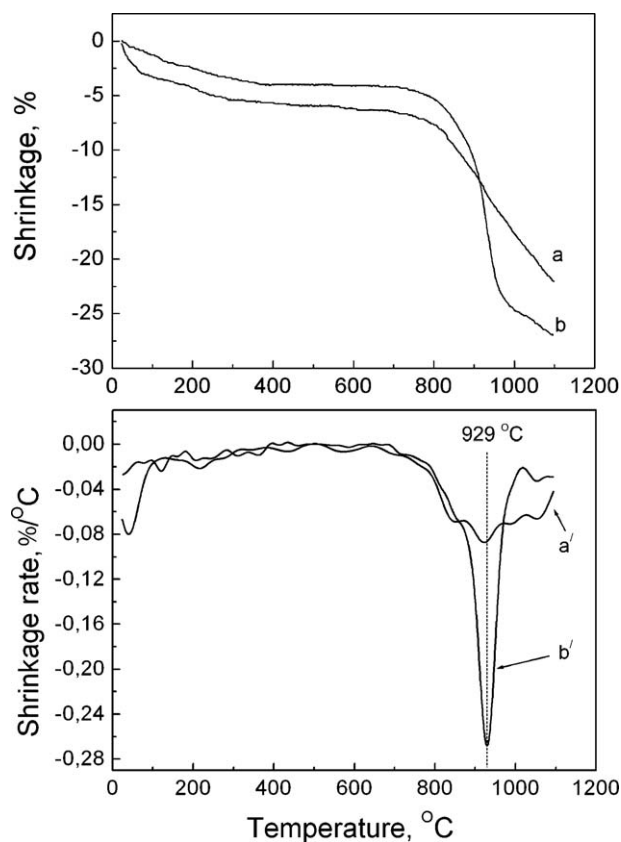


Fig. 3. Curves of the shrinkage and shrinkage rate for the compacts during heating in a, a' – air, and b, b' – the CO<sub>2</sub> flow.

with the characteristics of IR bands and 3.4 wt% CO<sub>3</sub><sup>2-</sup> content (Figs. 1c and 2a), the initial powder is a slightly carbonated B-type HA.<sup>23,24</sup>

The amount of CO<sub>2</sub> released from the powder in air (2.6 wt%) is the same like in N<sub>2</sub> (2.5 wt%) under equal conditions (Fig. 2b; the experimental error is  $\pm 0.1$  wt%). N<sub>2</sub> atmosphere (flow) and air have a negligible effect on the mass loss in the 600–1000 °C range. However, the CO<sub>2</sub> flow has. The total mass loss in the powder heated to 1200 °C in the CO<sub>2</sub> flow is 10.6 wt% (Fig. 2c), including 8.2 wt% mass loss from RT to 600 °C, 1.6 wt% from 600 to 1000 °C and 0.8 wt% for temperatures above 1000 °C, compared to the total 14.2 wt% mass loss in air, including 10.2 wt%, 2.7 wt% and 1.3 wt%. The amount of released CO<sub>2</sub> is almost two times less than that in air. It is assumed that the reduction in mass loss is caused by the formation of new CO<sub>3</sub><sup>2-</sup> groups formed by CO<sub>2</sub> molecules taken up from the flow. These new carbonates partly compensate those decomposed and released as CO<sub>2</sub> during heating. In that case, there still are 3.4 wt%–2.2 wt% = 1.2 wt% CO<sub>3</sub><sup>2-</sup> in the initial CHA powder heated to 1000 °C in the CO<sub>2</sub> flow.

### 3.2. Shrinkage of the powder compacts

Shrinkage of the powder compacts, containing 3.4 wt% CO<sub>3</sub><sup>2-</sup> initially, starts at about 700 °C while heating in air (Fig. 3a). The shrinkage rate increases with increasing temperature and reaches a maximum at about 930 °C and decreases

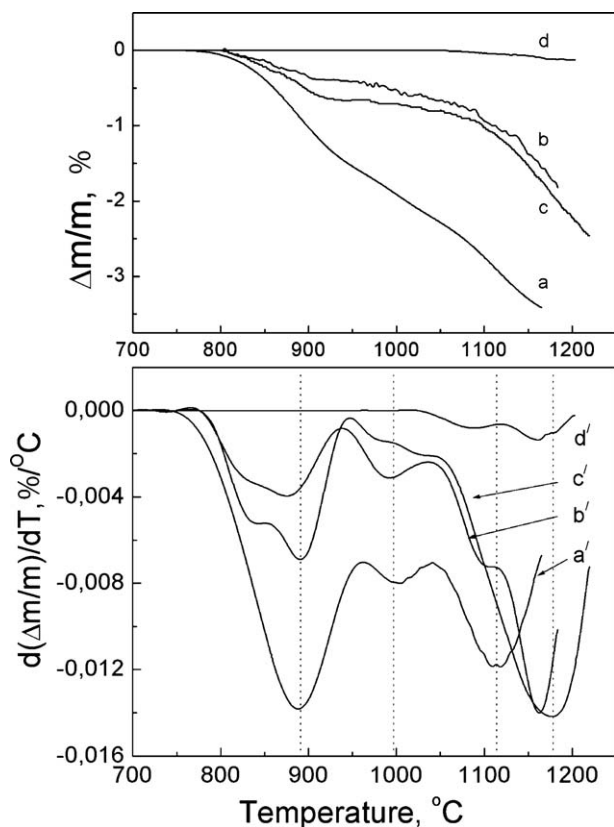


Fig. 4. TG and DTG curves of the compacts in air preliminary fired in the CO<sub>2</sub> flow for 2 h at a, a' – 800, b, b' – 900, c, c' – 1000 °C, and d, d' – 1100 °C.

afterwards at higher temperatures (Fig. 3a'). An impressive effect is observed in case of heating similar compacts in the CO<sub>2</sub> flow. The shrinkage commences and the shrinkage rate passes through a maximum at about the same temperatures as in air (Fig. 3b and b'). However, the maximum rate of shrinkage in CO<sub>2</sub> is more than three times higher than that in air. The beginning and the development of the shrinkage displayed on the temperature scale are consistent with the process of mass loss due to CO<sub>2</sub> liberation in N<sub>2</sub>. Moreover, the temperatures of the maximum rates of the gas release and the shrinkage almost coincide (922 and 929 °C, Figs. 2d and 3a', b').

CO<sub>2</sub> gas liberation from incompacted CHA powder may differ from that of compacted powder.<sup>11</sup> Also, shrinkage may not result in sintering.<sup>12,13</sup> Besides, the CHA powder displays less mass loss while heating in CO<sub>2</sub> as that in N<sub>2</sub> or air (Fig. 2). Considering this and the desire to strengthen the observed gas-activated effect and to develop an approximate heat-treatment for sintering, the compacts are fired in a CO<sub>2</sub> flow for 2 h at temperatures of 800, 900, 1000, 1100 and 1200 °C.

For compacts fired at 800 °C, the mass loss in the 800–1000 °C range in air is 1.9 wt% (Fig. 4a), i.e. higher than the 1.2 wt% of the initial powder (Fig. 2b). Consequently, some carbonation happens in the compacts during firing. The corresponding DTG curve (Fig. 4a') displays a maximum in the rate of mass loss at 890 °C. This temperature is somewhat lower than that of the maximum rate of shrinkage in the dilatometric test (Fig. 3b'). Temperatures of the maximum rate of

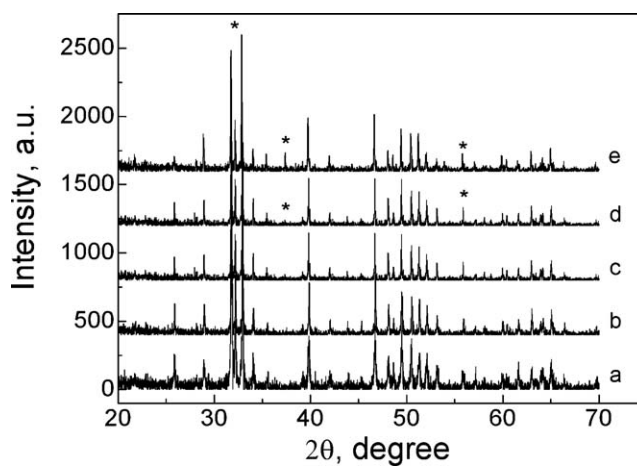


Fig. 5. XRD patterns of the compacts upon firing in the CO<sub>2</sub> flow for 2 h at a – 800, b – 900, c – 1000, d – 1100 °C, and e – 1200 °C.

shrinkage (sintering temperatures) in CHA powder compacts are found to decrease as the carbonate content in the initial powder increases.<sup>9,10</sup> Hence, the two temperatures of the maximum rates of shrinkage and mass loss (929 and 890 °C) can be considered as an indicator for the same process because the carbonate content in the compact fired at 800 °C is slightly higher than that in the initial powder. The other results in Fig. 4 are discussed further.

A minor acceleration is found in the shrinkage during heating the compacts in air (Fig. 3a'). The initial carbonate ions are decomposed almost completely, and the CO<sub>2</sub> molecules formed of the fractions are released from the lattice to 1000 °C. The N<sub>2</sub> and air atmospheres had negligible effect on this process (Figs. 2a, b and 3a'). However, while heating a compact in the CO<sub>2</sub> flow, a CO<sub>2</sub> uptake into the lattice takes place. There exist two opposite CO<sub>2</sub> streams, one into the bulk of particles, which resulted in the new CO<sub>3</sub><sup>2-</sup> formation, and another stemming from the particles because of the thermal CO<sub>3</sub><sup>2-</sup> decomposition in the lattice (as in air or N<sub>2</sub>). This partial exchange with CO<sub>2</sub> between the crystallites and the gaseous medium might have caused alterations in the amount and position of carbonates and, consequently, in the lattice characteristics.

### 3.3. Densification of the compacts fired in a CO<sub>2</sub> flow

XRD patterns show no changes in the phase composition for the compacts fired at 800, 900 and 1000 °C (Fig. 5a–c): exclusively characteristic CHA peaks appear. Only few CaO was formed in the samples fired at 1100 °C, and the CaO content slightly increases in the compacts fired at 1200 °C. This can be followed from the presence of very weak characteristic CaO reflections and a slight increase of their intensities in the corresponding patterns (Fig. 5d and e) besides the CHA peaks.

The increased sharpness of the diffraction profiles, compared to those in Figs. 1b and 5, enables the determination of the lattice constants for the fired compacts. The obtained values (Fig. 6) for the lattice constant *a*, the constant *c* showed slighter changes, of the material after firing the compacts at 800 and 900 °C are markedly lower than the 9.418 Å of stoichiometric HA.<sup>25</sup> Such a decrease is usually attributed to the CO<sub>3</sub><sup>2-</sup> substitution for

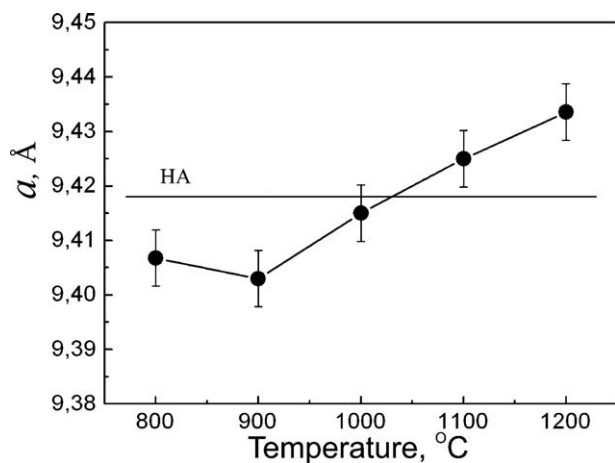


Fig. 6. The lattice constant  $a$  vs firing temperature of the CHA compacts.

$\text{PO}_4^{3-}$  ions.<sup>26</sup> The concentration of  $\text{CO}_3^{2-}$  on B-sites causes the observed decrease of  $a$  to 9.407 Å (800 °C) and 9.403 Å (900 °C) considering that  $\text{CO}_3^{2-}$  ions in the phosphate positions tend to reduce the  $a$ -parameter by 0.006 Å/wt%  $\text{CO}_3^{2-}$ .<sup>24,26,27</sup> The calculations show that  $(9.418-9.407 \text{ Å})/0.006 \text{ Å/wt}\% = 1.83 \text{ wt}\%$  and  $(9.418-9.403)/0.006 \text{ Å/wt}\% = 2.5 \text{ wt}\%$  of  $\text{CO}_3^{2-}$  occupy the B-sites after firing the compacts at 800 °C and 900 °C, respectively. Because the carbonate content in the initial powder after heating in the  $\text{CO}_2$  flow to 900 °C is (according to  $c$ -curve in Fig. 2) 3.4–1.6 wt% = 1.8 wt% (the  $\text{CO}_2$  mass loss was 1.15 wt%), it can be concluded that B-site carbonation occurs during firing the compacts at 900 °C. The picture radically changes for the compacts fired above 900 °C. The  $a$ -constant increases, and the values plotted versus temperature result in a nearly linear dependence (Fig. 6). This is typical for an A-type substitution in CHA when the  $\text{CO}_3^{2-}$  groups occupy the  $\text{OH}^-$  positions.<sup>26</sup>

IR spectra of the fired compacts (Fig. 7) confirm the XRD data and give additional information. In principal, an IR spectrum of the compact fired at 800 °C has the same characteristics as that of the initial powder (Figs. 7a and 1c). However, some

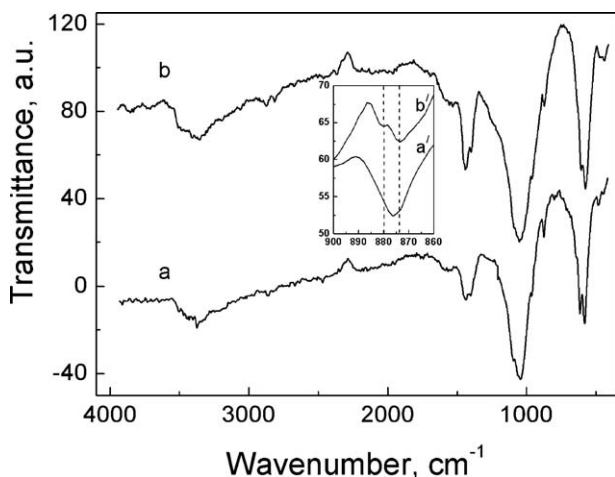


Fig. 7. IR spectra of the compacts fired in the  $\text{CO}_2$  flow for 2 h at a, a' – 800 °C, and b, b' – 1000 °C. The insert – an extended  $\nu_2 \text{CO}_3^{2-}$  range.

Table 1

Density ( $\rho$ ), Vickers microhardness ( $H_v$ ) and compressive strength ( $\sigma_c$ ) of the compacts fired at various temperatures ( $T_f$ ) for 2 h in the  $\text{CO}_2$  flow.

$T_f$ (°C)	$\rho$ (g/cm <sup>3</sup> )	$H_v$ ( $\pm 10\%$ ) (MPa)	$\sigma_c$ ( $\pm 10\%$ ) (MPa)
800	2.65 $\pm$ 0.01	127	219
900	2.88 $\pm$ 0.01	156	224
1000	2.97 $\pm$ 0.01	171	200
1100	2.23 $\pm$ 0.01	118	14
1200	2.26 $\pm$ 0.01	126	25

distinguishing features appear in spectra of the compacts fired at temperatures above 800 °C. For the compacts fired at 1000 °C (Fig. 7b), clear peaks and more or less resolved shoulders at 1410, 1450, 1460, 1475, 1500, 1515  $\text{cm}^{-1}$  and, particularly, at 1545 and 1570  $\text{cm}^{-1}$  in the  $\nu_3 \text{CO}_3^{2-}$  region are present indicating an AB-type CHA.<sup>6,28</sup> Instead of a sharp absorption at 875  $\text{cm}^{-1}$ , a doublet appears, though poorly resolved but clearly discerned, at 873 and 880  $\text{cm}^{-1}$  in the  $\nu_2 \text{CO}_3^{2-}$  region (the inset in Fig. 7). The ratio of the intensities of the peaks at 880 and 873  $\text{cm}^{-1}$ , corresponding to the ratio of A-type/B-type substitution,<sup>6</sup> is 0.49, indicating that there are insignificantly more carbonate groups on the B-site than on the A-site in the lattice. However, the ratio of the intensities increased to 0.95 for the ceramics fired at 1200 °C denoting that the relative amount of  $\text{CO}_3^{2-}$  on the A-sites increases, which is in full agreement with an increase of  $a$  in the 900–1200 °C firing range (Fig. 6). Another important feature is the broadening of the  $\text{PO}_4^{3-}$  bands as the firing temperature of the compacts is increased (Fig. 7a and b) which results in a gradual loss of resolution in the spectra. Such broadening is usually associated with a decrease in crystallinity of HA.<sup>29</sup> Most likely the broadening in the spectra of the compacts fired at and above 1000 °C is associated with the decrease in crystallinity because of the development of stresses in the lattice as the carbonate is known to cause distortions in the HA structure. Since the carbonate ions on A-positions distort the lattice more than on B-positions,<sup>22</sup> the crystallinity in the fired compacts decreases as the relative amount of the A-type substitution increases with an increase in firing temperature.

The microstructure, density and mechanical properties (microhardness and compressive strength) were studied to clarify how the shrinkage is associated with sintering in the fired compacts. The microstructure of a fractured compact after firing at 800 °C reveals powder particles fused together to a certain degree (Fig. 8a). The relative density of the compact is 84%, i.e. around 16% of the initial porosity in the compact (51%) are still present (Fig. 9 and the Table 1). The porosity decreases and both density and microhardness increase to maximum values as the firing temperature is increased to 1000 °C. The compacts transform into ceramics after firing at 1000 °C with their fractured surface showing grains of micron sizes with developed internal microstrains because of the distortions (Figs. 8b, c and 9; Table 1). Firing at temperatures above 1000 °C results in a drastic decrease in density and mechanical properties. This is associated with the occurrence and growth of tiny particles on the surfaces of grains (Fig. 8d). Elemental analysis of the powder samples gave a calcium content of 39.4 wt % and a phosphate content

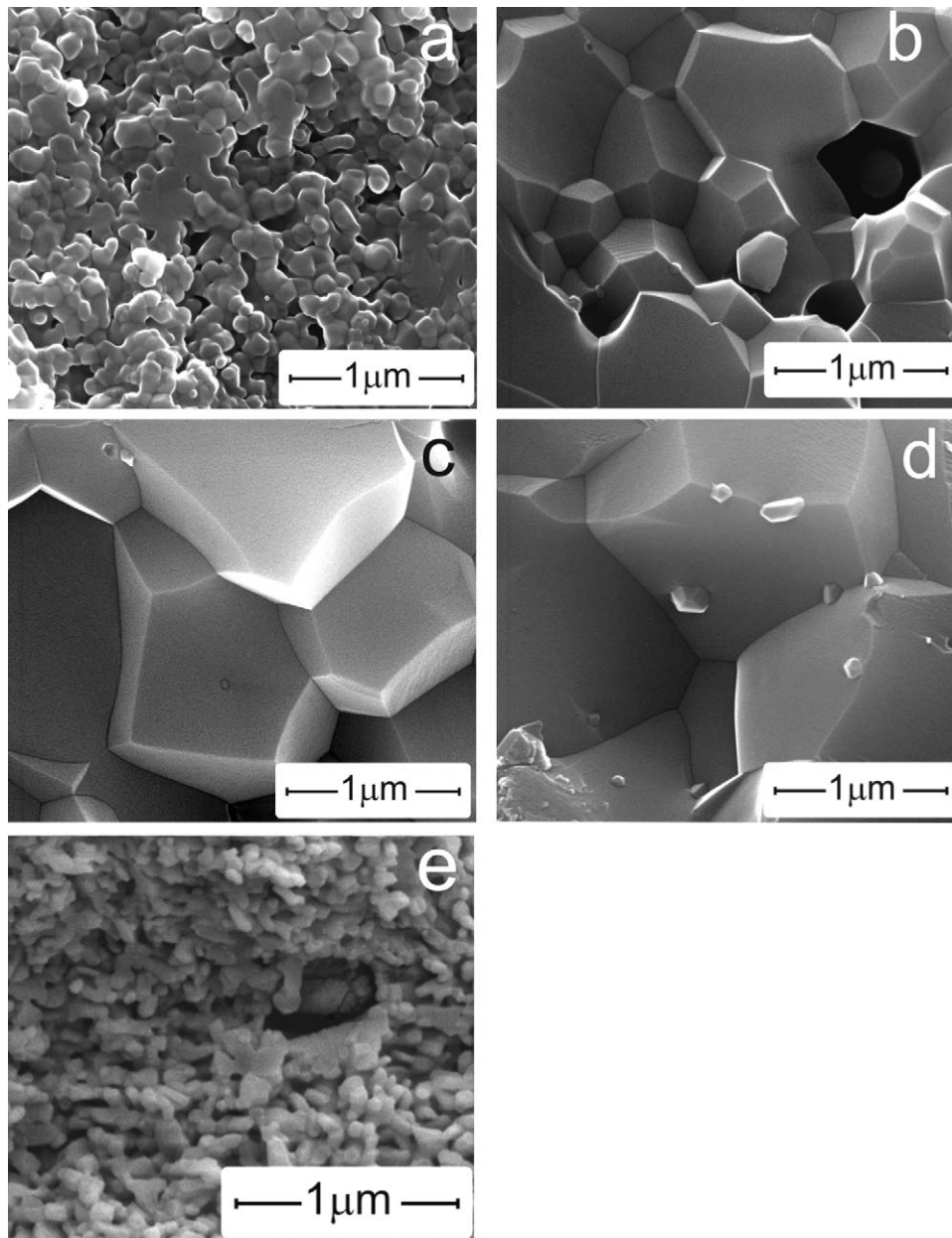


Fig. 8. The surface microstructure of the fractured compacts fired for 2 h in the  $\text{CO}_2$  flow at a – 800, b – 900, c – 1000, d – 1100 °C, and in air at e – 1000 °C.

of 52.4 wt % which corresponds to a Ca/P ratio of 1.79. Firing powder compacts with a ratio higher than the stoichiometric value of HA (1.67) at and above 1000 °C is known to result in the formation of CaO in the ceramics.<sup>30</sup> This is well consistent with the CaO reflections detected in the XRD patterns of the corresponding samples (Figs. 5d and e). The CaO particles most likely cause a loosening of the grain boundaries and weaken the ceramic.

The rapid shrinkage at 929 °C results in sintering and the formation of ceramics. Unfortunately, the effect of firing temperature on the characteristics of the sintered compacts is not detailed from 900 to 1000 °C. However, considering the assumed view of the density curve in this range (the dashed lines in Fig. 9), one might expect that the maximum density and the highest mechanical characteristics are actually achieved at a fir-

ing temperature between 900 and 1000 °C (around 985 °C), i.e. in the range of maximum activation of the shrinkage due to  $\text{CO}_2$  liberation. Contrary to this, the porosity is still open in the compacts fired at 1000 °C in air as can be seen in the micrographs (Fig. 8e). Since the sintering temperature of an AB-type CHA (the assumed value is 985 °C) is higher than that of a mainly B-type CHA (929 °C), it can be supposed that a CHA sintering temperature depends not only on the content but also on the mode of  $\text{CO}_3^{2-}$  distribution in the two lattice positions with a tendency to increase as the A/B ratio increases.

The obtained results contribute to a further clarification of the dependences in Fig. 4. As it is mentioned above, the porosity in the compacts after firing at 800 °C in the  $\text{CO}_2$ -flow is 16%, i.e. roughly one third of the initial porosity in the compacts (51%) is still present. Due to the remaining open porosity, about

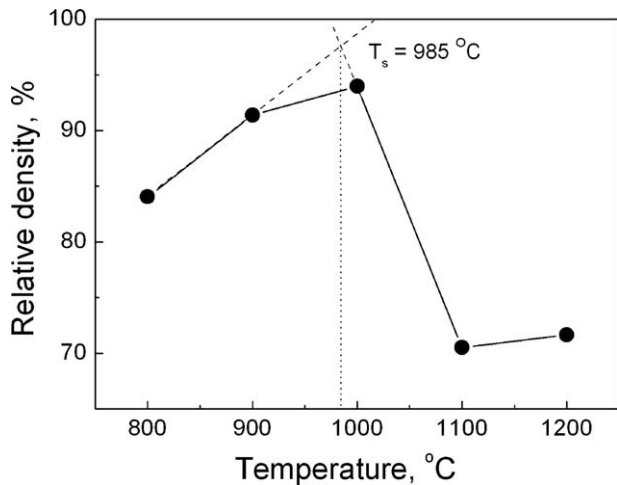


Fig. 9. The relative density vs temperature in the compacts fired for 2 h in the  $\text{CO}_2$  flow.

3.45 wt% of  $\text{CO}_2$  are released up to 1170 °C during a TG run (in air) from the compact (Fig. 4a). This mass loss results from the decomposition of 4.7 wt% of  $\text{CO}_3^{2-}$  in the lattice. The amount of the mass loss is an additional proof for the carbonation during firing the compact (the initial carbonate content in the powder is 3.4 wt%). Firing at 900 and 1000 °C yielded sintered ceramics because the residual porosities in the compacts are 9% and 6%, respectively (Fig. 9). As a consequence, the mass loss in both of them to 1170 °C is about 1.6 wt% of  $\text{CO}_2$  (Fig. 4b and c), i.e. more than twice as less than for the compact fired at 800 °C. The gas release from the compacts (ceramics) after firing at temperatures above 1000 °C decreases dramatically which is most likely attributed to the loss of the initial carbonate while heating to these high temperatures (Fig. 4d and d').

Three main maxima in gas release are observed at 890, about 1000, and in the 1110–1180 °C range for the compacts fired at 800, 900 and 1000 °C in the  $\text{CO}_2$  flow. The first maximum is attributed to the decomposition of  $\text{CO}_3^{2-}$  ions on the B-sites. The weak second one is mainly caused by the decomposition of carbonates on the A-sites and  $\text{CO}_2$  liberation from the almost fully dense grains. The third maximum in the high temperature range is supposed to appear because of the decomposition of the residual carbonates and, most likely, because of the loss of some  $\text{OH}^-$  groups. The density of the sintered ceramics decreases drastically after firing at temperatures above 1000 °C (Table 1 and Fig. 9), and this enables the liberation of the indicated pieces. The rate of mass loss at around 1170 °C is the same as that at 890 °C of the compact with open porosity which is an additional argument for the presented picture.

#### 4. Discussion

Based on the above results, a new supposition on the nature of the  $\text{CO}_2$ -activated sintering is proposed. Substantial activation in sintering happens at about 900 °C during firing the compacts in the  $\text{CO}_2$  atmosphere (Fig. 3). Simultaneously, the firing results in a carbonation of HA (mainly in B-sites; Fig. 6). Heating the compacts with different amounts of  $\text{CO}_3^{2-}$  in the

$\text{N}_2$ -atmosphere or air with no or a negligible amount of  $\text{CO}_2$  reveals a considerable rate of mass loss due to the decarbonation in the lattice at about 900 °C (Figs. 2d and 4a'–c'). Hence, there are two opposite  $\text{CO}_2$  streams while firing the compacts: the one goes from the  $\text{CO}_2$  atmosphere into the bulk of the apatite particles, and the other one the way round. Uptake and (or) release of  $\text{CO}_2$  molecules from the particles may activate the ion diffusion (likely, both the volume and the surface migrations) which results in sintering at much lower temperatures (around 900 °C) than usual for conventional HA sintering (1150–1200 °C<sup>1,2,19</sup>). However, the activation only proceeds at firing temperatures up to about 1000 °C. At higher temperatures, the carbonation takes part on the A-sites (Figs. 6 and 7). This leads to a filling of the hexed channels and blocks (restricts) with a release of decomposed  $\text{CO}_3^{2-}$  molecules from the lattice. As a result, the activation process is weakened drastically.

Proceeding on this supposition on the nature of the  $\text{CO}_2$  gas-activated sintering, a different view on some earlier findings in sintering CHA's can be proposed. For instance, a decrease in sintering temperature with an increase of carbonate content in an initial CHA powder was associated with simultaneous dispersion of the powder.<sup>10</sup> The dispersion may actually stimulate sintering due to the increased role of the surface diffusion. However, significantly different sintering temperatures were found for the same carbonation (and, consequently, similar dispersity) in CHA compacts in another study.<sup>9</sup> Based on our supposition, the discrepancy can be explained by the use of different sintering atmospheres in the studies, namely  $\text{CO}_2$  vaporized with water<sup>9</sup> and a flow of dry Ar.<sup>10</sup> The strong effect of the kind of gas atmosphere on the  $\text{CO}_3^{2-}$  loss in a CHA and, consequently, on the  $\text{CO}_2$  stream intensity at a definite (sintering) temperature is clearly seen in Fig. 3. According to another finding,<sup>11</sup> the decrease in sintering temperature is attributed to an increasing amount of sodium substituted for calcium with an increase in carbonate content. Sodium is supposed to form an easily melting compound promoting the shrinkage. However, a decrease of about 230 °C in the sintering temperature in dry  $\text{CO}_2$  compared to that in air was observed in this study (Fig. 3), when no sodium containing parent reagents were used for the synthesis. Finally, peculiarities in the shrinkage curve in the 700–1000 °C firing range in air are observed for compacts having similar dispersities but differing in the  $\text{CO}_3^{2-}$  contents.<sup>17</sup> The peculiarities are strongly associated with the gas release (mass loss) of the compacts. Compacts of pure HA usually have a smooth shrinkage curve.

#### 5. Conclusions

Densification of compacts of slightly carbonated hydroxyapatite nanoparticles under conditions of heating from RT to 1200 °C is highly effected by a  $\text{CO}_2$  gas flow in the 600–1000 °C range. Air and flowing  $\text{N}_2$  had slight and negligible effects on the densification. However, the flow of dry  $\text{CO}_2$  promotes an increase in the shrinkage rate of the compacts at 929 °C thrice as high. A mass loss in the compacts accompanies the densification. The mass loss is caused by the release of  $\text{CO}_2$  owing to the decomposition of carbonates on the B-sites in the CHA lattice.

Firing the compacts in the CO<sub>2</sub> flow at 800, 900 and 1000 °C for 2 h yields an increase in the carbonate content in the fired compacts and almost dense ceramics (after firing at 1000 °C). Depending on the treatment conditions, the sintering temperature of the compacts decreases by 260 °C: from about 1150 °C in air of HA to 890 °C in the CO<sub>2</sub> flow of CHA. The CHA ceramics have mechanical characteristics suitable for a use as medical implants. Similar firing of the compacts at temperatures above 1000 °C results in ceramics with an increase of carbonation on the A-sites. However, these ceramics show a drastic decrease in density and mechanical properties.

A new supposition on the nature of the CO<sub>2</sub> gas-activated sintering that partially results in the decrease of the sintering temperature has been proposed. According to the supposition, the CO<sub>2</sub> streams from the CO<sub>2</sub> atmosphere into the bulk and (or) vice versa, owing to the CO<sub>3</sub><sup>2-</sup> decomposition in the lattice, activate the diffusion processes in the CHA nanoparticles and promote sintering.

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